

Q.5. Determine the following for the voltage dividing bias network of Figure 5

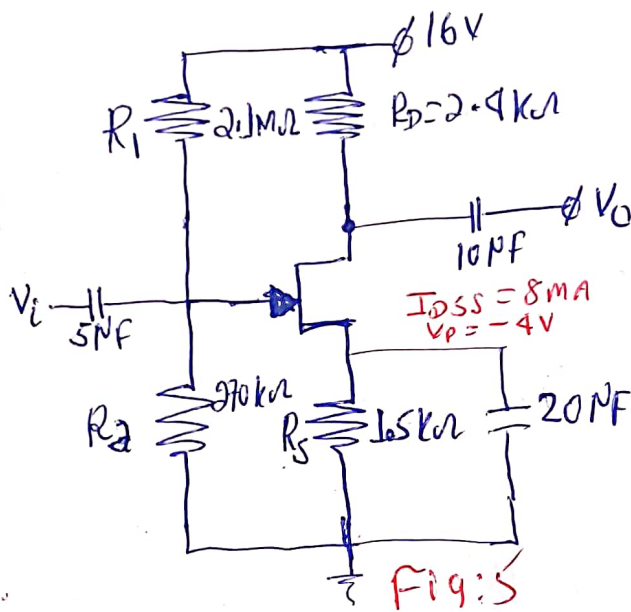
a)  $I_{DQ}$  &  $V_{GSQ}$

b)  $V_D$

c)  $V_S$

d)  $V_{DS}$

e)  $V_{DG}$



Soln Compute the Thevenin's Equivalent cct.

$$V_{TH} = V_{GG} = \frac{R_2}{R_1 + R_2} V_{DD} = \frac{270k\Omega}{210k\Omega + 270k\Omega} \times 16V$$

$$= \frac{270k\Omega}{2370k\Omega} \times 16V = 1.82V$$

$$R_{TH} = \frac{R_1 \times R_2}{R_1 + R_2} = \frac{210 \times 270}{2370} = 239.24k\Omega$$

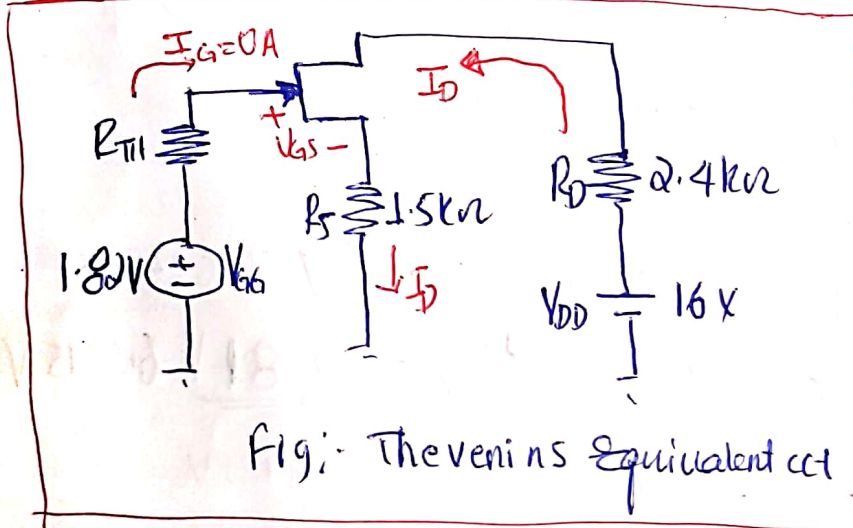


Fig:- Thevenin's Equivalent cct

\* Apply KVL for the  $I_D$  loop

$$V_{GG} - I_G R_{TH} - V_{GS} - I_D R_S = 0$$

$$\Rightarrow V_{GS} = V_{GG} - I_D R_S$$

$$V_{GS} = 1.82V - 1.5I_D$$

\* Now use Shockley's Eqn to find  $I_D$

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2$$

$$I_D = 8 \left(1 - \frac{1.82 - 1.5I_D}{-4}\right)^2$$

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$$I_D = 8 \left( 1 + \frac{1.82 - 1.5 I_D}{4} \right)^2 = 8 \left( \frac{5.82 - 1.5 I_D}{4} \right)^2$$

$$I_D = \frac{8}{16} (5.82 - 1.5 I_D)^2 = \frac{1}{2} \left\{ 33.8724 - 17.46 I_D + 2.25 I_D^2 \right\}$$

$$I_D = 16.9362 - 8.73 I_D + 1.125 I_D^2$$

$$\Rightarrow 1.125 I_D^2 - 9.73 I_D + 16.9362 = 0$$

$$I_D^2 - 8.65 I_D + 15.0544 = 0$$

$$I_D = \frac{8.65 \pm \sqrt{8.65^2 - 4 \times 15.0544}}{2} = \frac{8.65 \pm 3.82}{2}$$

$$= 6.235 \text{ mA or } 2.415 \text{ mA}$$

Since both the solutions are less than  $I_{DSS}$ , Compute  $V_{GS}$  using both values & see for contradiction.

using  $I_D = 6.235 \text{ mA}$

$$\begin{aligned} V_{GS} &= 1.82 - 1.5I_D \\ &= 1.82 - 1.5 \times 6.235 \\ &= -7.5325 \text{ V} \end{aligned}$$

⇒ Invalid since  $V_{GS} < V_p$

Using  $I_D = 2.415 \text{ m}^4$

$$\begin{aligned} V_{GS} &= 1.82 - 1.5 I_D \\ &= 1.82 - 1.5 \times 2.415 \\ &= -1.8025 \text{ V} \end{aligned}$$

Valid since  $V_{GS} > V_p$

$$b) V_D = V_{DD} - I_D R_D = 16V - 2.415mA \times 2.4k\Omega$$
$$= 16V - 5.796V = \underline{\underline{10.204V}}$$

c)  $V_S = I_D R_S = 2.415 \text{ mA} \times 1.5 \text{ k}\Omega = 3.6225 \text{ V}$

$$d) V_{DS} = V_D - V_S = (10.204 - 3.619) V = \underline{\underline{6.585 V}}$$

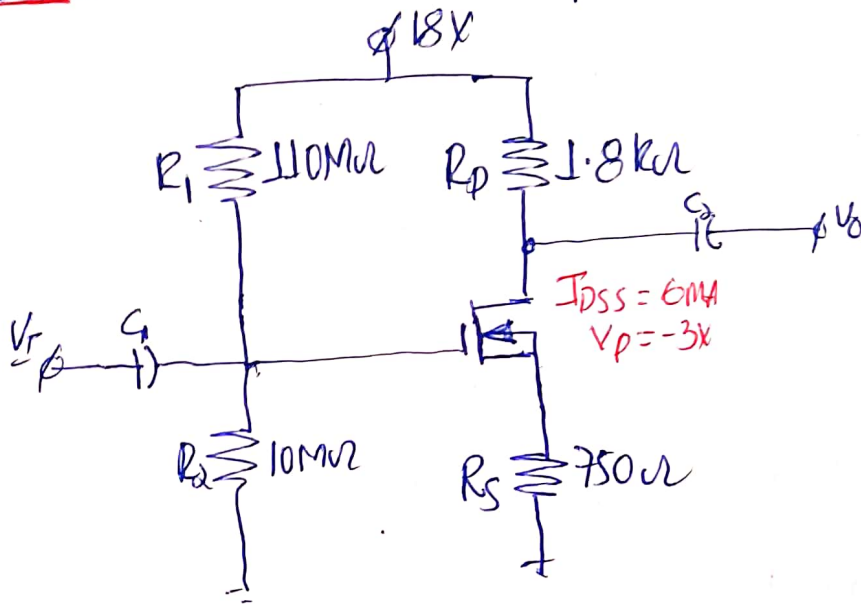
e)  $W_{Gr} = V_{Gr} + V_s = (-1.8025 + 3.675) V \hat{=} 1.8725 V$

$$V_G = V_{GG} = 1.82 \text{ V}$$

Or  $V_G = V_{GS} + V_S = -1.8025V + 3.6225V = 1.82V$

No realme - Shot on realme - C257V = 8.384V

**Q.6** For the n-channel depletion type MOSFET of Fig 6, determine



- a)  $I_{DQ}$  &  $V_{GSQ}$   
b)  $V_{DS}$

Soln

$$V_G = \frac{R_2}{R_1 + R_2} V_{DD} = \frac{10}{110 + 10} \times 18V = 1.5V$$

applying KVL for the g-s loop

$$V_G - V_{GS} - I_D R_S = 0$$

$$V_{GS} = V_G - I_D R_S = 1.5V - 0.75 I_D$$

Using Shockley's Equation

$$I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2 = 6 \left( 1 - \left[ \frac{1.5 - 0.75 I_D}{-3} \right] \right)^2$$

$$= 6 \left\{ 1 + \frac{1.5 - 0.75 I_D}{3} \right\}^2 = 6 \left( 1 + 0.5 - 0.25 I_D \right)^2$$

$$= 6 \left( 1.5 - 0.25 I_D \right)^2 = 6 \left( \frac{6 - I_D}{4} \right)^2$$

$$I_D = \frac{6}{16} (6 - I_D)^2$$

$$\frac{16}{6} I_D = 36 - 12 I_D + I_D^2$$

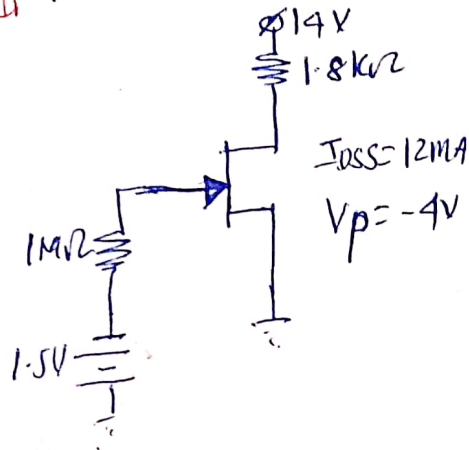
$$I_D^2 - 14.67 I_D + 36 = 0$$

Solving the Quadratic Equation

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# FIXED BIAS EXAMPLE

Q1. For the Fixed bias configuration shown

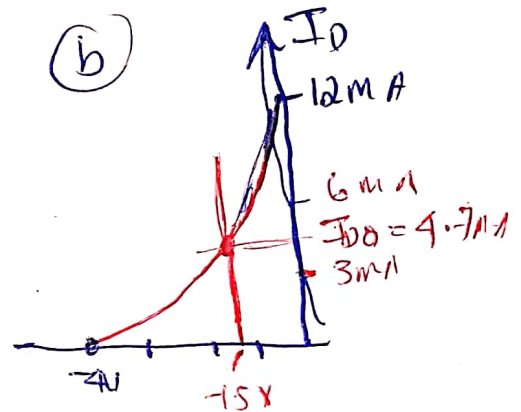


- Sketch the transfer characteristic of the device
- Superimpose the n/w equation on the same graph
- determine  $I_{DQ}$  &  $V_{DSQ}$
- Using Shockley's Equation, solve for  $I_{DQ}$  &  $V_{DSQ}$ . Compare the solutions of part c

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- a)  $V_{GS} = 0V, I_D = I_{DSS} = 12mA$   
 $V_{GS} = V_P = -4V, I_D = 0mA$   
 $V_{GS} = \frac{V_P}{2} = -2V, I_D = \frac{I_{DSS}}{4} = 3mA$   
 $V_{GS} = 0.3V_P = -1.2V, I_D = \frac{I_{DSS}}{9} = 6mA$

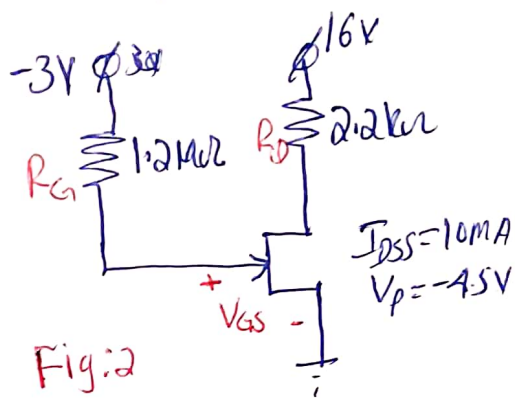


c)  $I_{DQ} = 4.7mA$   
 $V_{DSQ} = V_{DD} - I_{DQ} R_D = 14V - (4.7mA)(1.8k\Omega)$   
 $= \underline{5.54V}$

d)  $I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2 = 12mA \left(1 - \frac{(-1.5V)}{-4V}\right)^2$   
 $= 12mA \left(1 - \frac{1.5}{4}\right)^2 = 12mA \times \frac{25}{64} = 4.6875mA$   
 $\approx 4.69mA$

$V_{DSQ} = V_{DD} - I_{DQ} R_D$   
 $= 14V - (4.69mA)(1.8k\Omega)$   
 $= 5.56V$

Q.2 For the fixed bias configuration of JFET, determine



- $I_{DS}$  &  $V_{GS}$  using a purely mathematical approach
- Repeat 'a' using a graphical approach & compare results
- $V_{DS}$ ,  $V_D$ ,  $V_G$  &  $V_S$  using the results of part 'a'

Soln  $I_G = 0A$

@ Using KVL for the gdp loop

$$-3V - I_G \times R_G - V_{GS} = 0$$

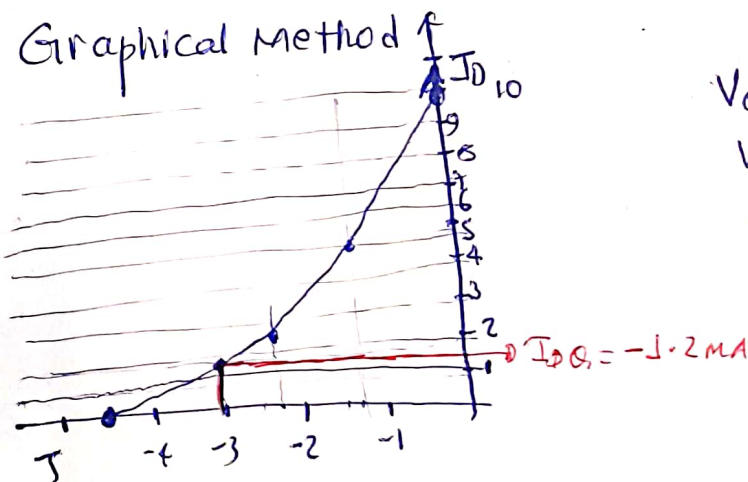
$$-3V - V_{GS} = 0$$

$$\underline{V_{GS} = -3V}$$

using Shockley's Eqn

$$\begin{aligned} I_D &= I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2 \\ &= 10mA \left(1 - \frac{-3V}{-4.5V}\right)^2 \\ &= 10mA \left(1 - \frac{3}{4.5}\right)^2 \\ &= 10mA \left(1 - \frac{2}{3}\right)^2 = \frac{10}{9}mA \\ &= 1.11mA \end{aligned}$$

b) Graphical Method



$$V_{GS} = 0V, I_D = 10mA$$

$$V_{GS} = \frac{V_P}{3} = -1.5V, I_D = 2.5mA$$

$$V_{GS} = 0.3V_P = -1.35V, I_D = 5mA$$

c) using KVL in the ddp loop

$$16V - I_D R_D - V_{DS} = 0$$

$$16V - 1.11mA \times 2.2k\Omega - V_{DS} = 0$$

$$\begin{aligned} V_{DS} &= 16V - 1.11 \times 2.2V \\ &= 16V - 2.442V = 13.558V \end{aligned}$$

$$V_D = V_{DS} = 13.558V$$

$$V_G = V_{GS} = -3V$$

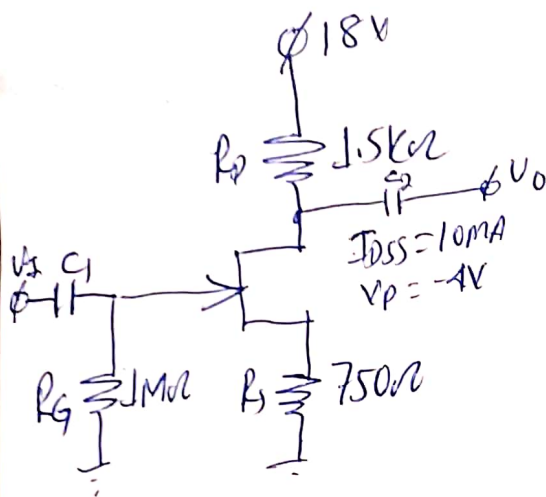
$$V_S = 0V$$

## SELF BIAS

Q.3 For the self bias configuration

a)  $I_{DQ}$  &  $V_{GSQ}$

b)  $V_{DS}$ ,  $V_{D1}$ ,  $V_G$  &  $V_S$



Soln using KVL for the ~~dc~~ loop

$$-V_{GS} - I_D R_S = 0$$

$$V_{GS} = -I_D R_S = -750 I_D = -0.75 I_D, \quad I_D \text{ in mA}$$

using Shockley's Eqn

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2 = 10 \left(1 - \frac{-0.75 I_D}{-4}\right)^2$$

$$I_D = 10 \left(1 - \frac{1.5 I_D}{4} + \frac{0.75^2 I_D^2}{4^2}\right)$$

$$I_D = 10 - 3.75 I_D + 0.352 I_D^2$$

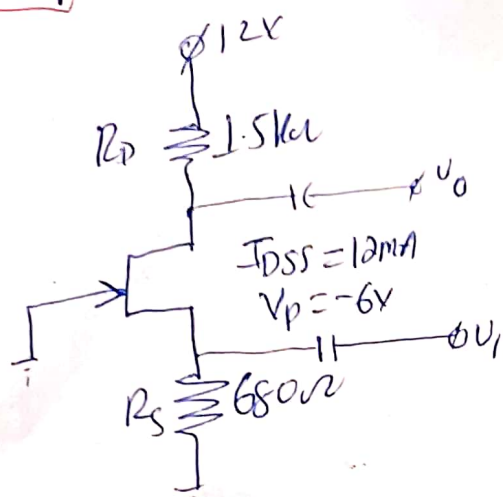
$$0.352 I_D^2 - 4.75 I_D + 10 = 0$$

$$I_D^2 - 13.49 I_D + 28.41 = 0$$

$$I_D = \frac{13.49 \pm \sqrt{13.49^2 - 4 \times 28.41}}{2} = \frac{13.49 \pm \sqrt{181.9801 - 113.64}}{2}$$

$$= \frac{13.49 \pm \sqrt{68.3401}}{2} = \frac{13.49 \pm 8.27}{2} = \frac{21.76}{2} \text{ or } \frac{5.22}{2}$$

Q.1<sup>3</sup> Determine the following for the common-gate configuration.



a)  $V_{GSQ}$

b)  $I_{DQ}$

c)  $V_D$

d)  $V_G$

e)  $V_S$

f)  $V_{DS}$

Soln  $V_{GS} = -I_D R_S = -0.68 I_D$

$$I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2 = 12 \left( 1 - \left( \frac{-0.68 I_D}{-6V} \right) \right)^2$$

$$= 12 (1 - 0.113 I_D)^2$$

$$I_D = 12 - 2.712 I_D + 0.1532 I_D^2$$

$$0.1532 I_D^2 - 3.712 I_D + 12 = 0$$

$$I_D^2 - 24.23 I_D + 78.33 = 0$$

$$I_D = \frac{24.23 \pm \sqrt{(24.23)^2 - 4 \times 78.33}}{2}$$

$$= \frac{24.23 \pm 16.55}{2} = 20.39 \text{ mA or } 3.84 \text{ mA}$$

↓  
Invalid

↓  
Valid

$$V_{GS} = -0.68 I_D = -0.68 \times 3.84 = -2.6112 \text{ V}$$

c)  $V_D = V_{DD} - I_D R_D = 12V - 3.84 \text{ mA} \times 1.5 \text{ k}\Omega$   
 $= 6.24 \text{ V}$

d)  $V_G = 0 \text{ V}$

e)  $V_S = I_D R_S = 3.84 \text{ mA} \times 0.68 = 2.6112 \text{ V}$

f)  $V_{DS} = V_D - V_S = 6.24 \text{ V} - 2.6112 \text{ V} = 3.6288 \text{ V}$

compute  $V_{GS}$  for both values of  $I_D$  & rule out the valid solution

For  $I_D = 3.115 \text{ mA}$

$$\begin{aligned} V_{GS} &= 1.5 - 0.75 I_D \\ &= 1.5 - 0.75 \times 3.115 \\ &= -0.83625 \text{ V} \end{aligned}$$

Valid since  $V_{GS} > V_p$

For  $I_D = 11.555 \text{ mA}$

$$\begin{aligned} V_{GS} &= 1.5 - 0.75 \times I_D \\ &= 1.5 - 0.75 \times 11.555 \\ &= -7.16625 \text{ V} \end{aligned}$$

Invalid since  $V_{GS} < V_p$

Therefore, the correct value of  $I_D$  is  $3.115 \text{ mA}$

$$I_{DQ} = 3.115 \text{ mA}$$

$$V_{GS} = -0.83625 \text{ V} \approx \underline{\underline{-0.84 \text{ V}}}$$

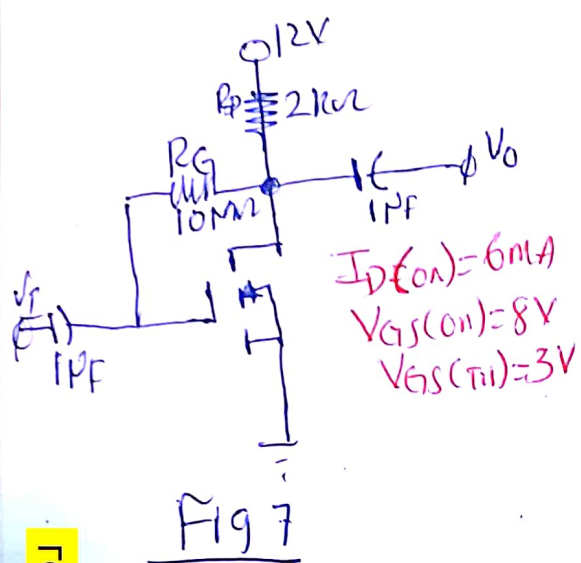
using KVL in the o/p loop

$$V_{DD} - I_D R_D - V_{DS} - I_D R_S = 0$$

$$\begin{aligned} V_{DS} &= V_{DD} - I_D (R_D + R_S) \\ &= 18 \text{ V} - 3.115 \text{ mA} \times (1.8 \text{ k}\Omega + 0.75 \text{ k}\Omega) \\ &= 18 \text{ V} - 3.115 \text{ mA} \times 2.55 \text{ k}\Omega \\ &= 18 \text{ V} - 7.94325 \text{ V} \\ &= \underline{\underline{10.06 \text{ V}}} \end{aligned}$$

Q.7

Determine  $I_{DQ}$  &  $V_{DSQ}$  for Enhancement-type MOSFET shown in Fig 7



Soln

$$K = \frac{I_D(on)}{(V_{GS(on)} - V_{GS(th)})^2}$$

$$= \frac{6mA}{(8V - 3V)^2} = 0.24 \frac{mA}{V^2}$$

Since no-current flows through  $R_G$ ,  $V_D$  &  $V_S$  are equal

$$V_{DD} - I_D R_D - V_{DS} = 0$$

$$V_{DS} = V_{DD} - I_D R_D = 12 - 2I_D$$

Now using the  $I_D$  Expression

$$I_D = K (V_{GS} - V_T)^2$$

$$= 0.24 (12 - 2I_D - 3)^2 = 0.24 (9 - 2I_D)^2$$

$$= 0.96 (4.5 - I_D)^2$$

$$1.042 I_D = (4.5 - I_D)^2 = I_D^2 - 9I_D + 20.25$$

$$I_D^2 - 10.042 I_D + 20.25 = 0$$

Solving for  $I_D$

$$I_D = 1.9mA \text{ or } I_D = 11.942mA$$

$$I_D = \frac{10.042 \pm 4.454}{2} = 2.7938mA \text{ or } 7.2482mA$$

To get the valid value of  $I_D$ , compute  $V_{GS}$

For  $I_D = 2.7938mA$

$$V_{GS} = 12 - 2I_D$$

$$= 12 - 2 \times 2.7938$$

$$= 6.4124V$$

Valid Since  $V_{GS} > 3V$

For  $I_D = 7.2482mA$

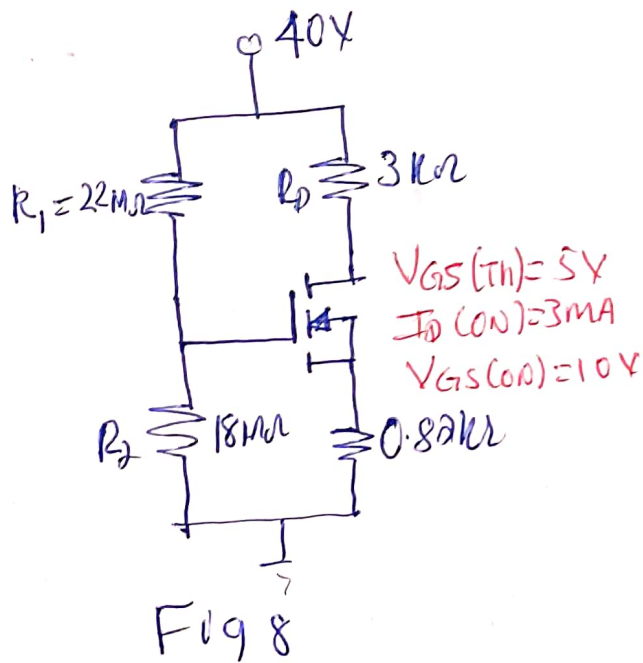
$$V_{GS} = 12 - 2 \times 7.2482$$

$$= -2.4964V$$

Invalid b/c  $V_{GS} > 3V$

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Q.8 Determine  $I_{DQ}$ ,  $V_{GSQ}$  &  $V_{DS}$  for the n/w of Fig 8



Solve

$$K = \frac{I_D(\text{on})}{(V_{GS}(\text{on}) - V_{GS}(\text{th}))^2}$$

$$= \frac{3 \text{ mA}}{(10\text{V} - 5\text{V})^2} = \frac{3}{25} \text{ mA/V}^2$$

$$= 0.12 \text{ mA/V}^2$$

Since  $I_G = 0 \text{ mA}$ ,  $V_G$  can be found as

$$V_G = \frac{R_2}{R_1 + R_2} V_{DD}$$

$$V_G = \frac{18}{40} \times 40\text{V} = 18\text{V}$$

Applying KVL for the g/s loop

$$V_G - V_{GS} - I_D R_S = 0$$

$$V_{GS} = V_G - I_D R_S = 18 - 0.82 I_D$$

Now using the  $I_D$  Equation

$$I_D = K (V_{GS} - V_{TH})^2$$

$$I_D = 0.12 (18 - 0.82 I_D - 5)^2$$

$$I_D = 0.12 (13 - 0.82 I_D)^2$$

$$I_D = 20.28 - 2.5584 I_D + 0.081 I_D^2$$

$$0.081 I_D^2 - 3.5584 I_D + 20.28 = 0$$

$$I_D^2 - 43.93 I_D + 250.37 = 0$$

⇒ Solving for  $I_D$

$$I_D = \frac{43.93 \pm 30.47}{2} = 6.73 \text{ mA} \quad \text{Valid}$$

or  $37.2 \text{ mA}$  not valid

Now solve for  $V_{GS}$

$$V_{GS} = 18 - 0.82 I_D$$

$$= 18 - 0.82 \times 6.73$$

$$\approx 12.48 \text{ V}$$

Applying KVL for the d/s loop

$$V_{DS} = V_{DD} - I_D (R_D + R_S)$$

$$= 40\text{V} - 6.73 \times 3.82$$

$$= 14.2914 \text{ V}$$

**Q.9** For the network of Fig 9, Determine

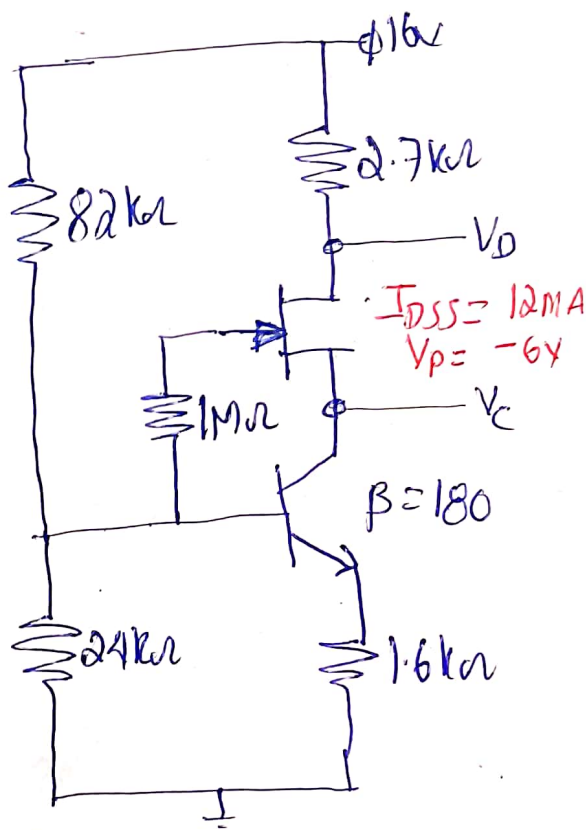


Fig 9

- $V_B$  &  $V_G$
- $V_E$
- $I_E, I_C$  &  $I_D$
- $I_B$
- $V_C, V_S$ , &  $V_D$
- $V_{CE}$
- $V_{DS}$

Soln  $V_{TH} = \frac{R_2}{R_1 + R_2} V_{DD} = \frac{24}{82 + 24} \times 16V \approx 3.62V$

$R_{TH} = R_1 || R_2 = 18.57k\Omega$

For a voltage divider bias,  $I_B$  is given as

$$I_B = \frac{V_{TH} - 0.7}{R_{TH} + (\beta + 1)R_E} = \frac{3.62V - 0.7V}{18.57k\Omega + 181 \times 1.6k\Omega}$$

$I_B = 9.47\mu A$

$I_C = \beta I_B = 180 \times 9.47\mu A = 1.70mA$

$I_E = (\beta + 1)I_B = 181 \times 9.47\mu A = 1.71mA$

$V_E = I_E R_E = 1.71mA \times 1.6k\Omega = 2.736V$

$V_B = V_{BE} + V_E = 0.7V + 2.736V = 3.436V$

Since  $I_G = 0mA$ ,  $V_B = V_G = 3.436V$

$I_D = I_C = 1.70mA$

$$V_D = V_{DD} - I_D R_D = 16V - 1.70mA \times 2.7k\Omega = 11.41V$$

Now compute  $V_{GS}$  using Shockley's Eq<sup>n</sup>

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2$$

$$V_{GS} = V_P \left(1 - \sqrt{\frac{I_D}{I_{DSS}}}\right) = V_P \left(1 - \sqrt{\frac{1.70mA}{12mA}}\right)$$

$$= 0.624 V_P = 0.624 \times (-6) = -3.744V$$

$$V_{GS} = V_G - V_S = V_B - V_C$$

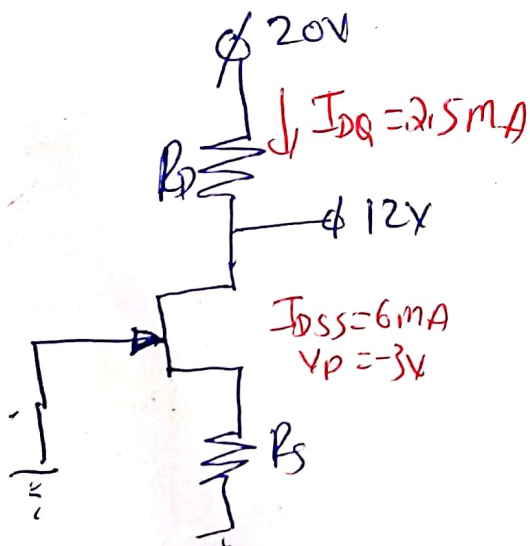
$$\Rightarrow V_C = V_B - V_{GS} = 3.436V + 3.744V = 7.18V$$

$$V_C = V_S = 7.18V$$

$$V_{CE} = V_C - V_E = 7.18V - 2.736V = \underline{4.444V}$$

$$V_{DS} = V_D - V_S = 11.41V - 7.18V = \underline{4.23V}$$

Q.10 For the n/w of Fig 10, the levels of  $V_{DSQ}$  &  $I_{DQ}$  are specified. Determine  $R_D$  &  $R_S$



Soln  $R_D = \frac{20V - 12V}{2.5mA} = 3.2k\Omega$

Use Shockley's Eq<sup>n</sup> to solve for  $V_{GS}$

$$\begin{aligned} V_{GS} &= V_P \left(1 - \sqrt{\frac{I_D}{I_{DSS}}}\right) \\ &= -3V \left(1 - \sqrt{\frac{2.5}{6}}\right) = \\ &= -3V \times 0.3545 \\ &= \underline{-1.064V} \end{aligned}$$

$$V_{GS} = -I_D R_S$$

$$R_S = \frac{-V_{GS}}{I_D} = \frac{-1.064V}{2.5mA} = \underline{425.6\Omega}$$